

ECE 3040B Microelectronic Circuits

Exam 2

July 3, 2001

Dr. W. Alan Doolittle

Print your name clearly and largely:

Solutions

Instructions:

Read all the problems carefully and thoroughly before you begin working. You are allowed to use 1 new sheet of notes (1 page front and back), your note sheet from the previous exam as well as a calculator. There are 100 total points in this exam. Observe the point value of each problem and allocate your time accordingly. **SHOW ALL WORK AND CIRCLE YOUR FINAL ANSWER WITH THE PROPER UNITS INDICATED.** Write legibly. If I can not read it, it will be considered to be a wrong answer. Do all work on the paper provided. Turn in all scratch paper, even if it did not lead to an answer. Report any and all ethics violations to the instructor. Good luck!

Sign your name on ONE of the two following cases:

I DID NOT observe any ethical violations during this exam:

I observed an ethical violation during this exam:

First 25% Multiple Choice (Select the most correct answer)

1.) (5-points) When analyzing a circuit using the ideal diode model, which of the following is true:

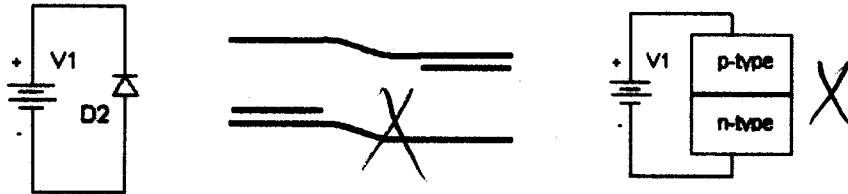
- a.) The diode is replaced with either an open or a short circuit
- b.) The diode is replaced with a battery plus an open or short circuit
- c.) The diode has a small non-zero leakage current flowing in reverse bias
- d.) The diode has an offset voltage equal to the built in voltage of the diode
- e.) None of the above.

2.) (5-points) The emitter injection efficiency, γ ...

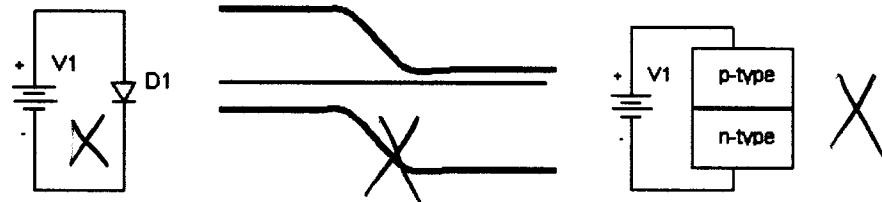
- a.) ...characterizes the ability of a diode to handle large currents.
- b.) ...characterizes the ability of a transistor to handle large currents.
- c.) ... characterizes the percentage of minority carriers in the base that make it to the collector.
- d.) ... characterizes how effectively the emitter can inject carriers into the base
- e.) ... characterizes how effectively the collector can inject carriers into the base

3.) (5-points) Which of the following bias diagrams is consistent with reverse bias (all three diagrams must be correct, i.e. the schematic symbols, energy band diagrams and the material drawing must have the correct polarity)?

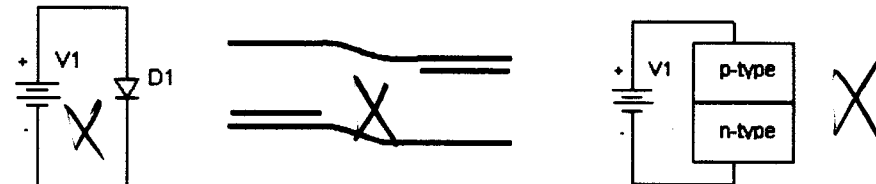
a.)



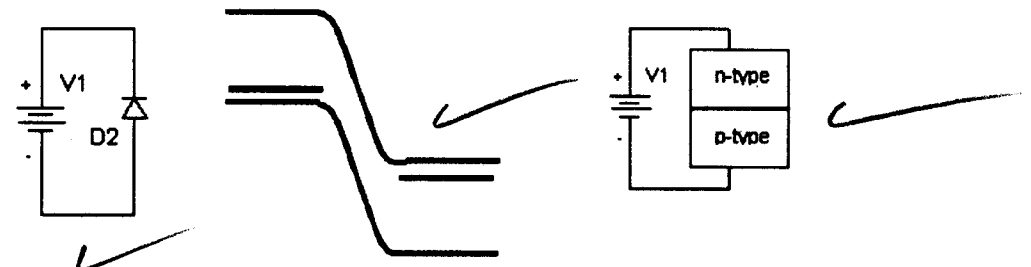
b.)



c.)

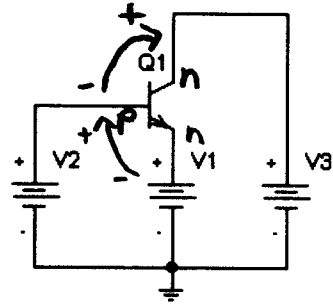


d.)



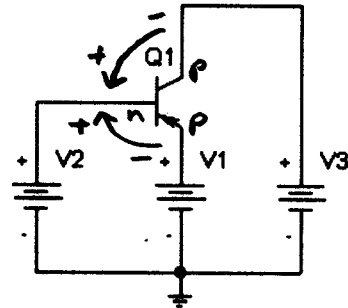
4.) (5-points) If we want to bias this transistor into forward active mode, which of the following is true?

- a.) $V_3 > V_2 > V_1$
- b.) $V_1 > V_2 > V_3$
- c.) $V_2 > V_1 > V_3$
- d.) $V_1 > V_3 > V_2$
- e.) You cannot bias a transistor without resistors.



5.) (5-points) If we want to bias this transistor into cutoff, which of the following is true?

- a. $V_3 > V_1$ and $V_1 > V_3$
- b. $V_1 > V_2$ and $V_3 > V_2$
- c. $V_2 > V_3$ and $V_1 > V_3$
- d. $V_2 > V_1$ and $V_2 > V_3$
- e. You cannot bias a transistor without resistors.



Second 15% Short Answer and Fill in the blank:

6.) (3-points each, 15 points total) The (a.) emitter of a BJT

biased into forward active mode is (b. circle one) Lightly / Heavily doped and is responsible for injecting its majority carriers into the

(c.) base where they diffuse to the

(d.) collector and are "collected" by a large

(e.) electric field.

Third 20%

7.) (20-points total in two parts) A GaAs p+ n diode has the following parameters:

Intrinsic concentration $n_i = 2 \times 10^6 \text{ cm}^{-3}$

Relative dielectric constant, K_s (or ϵ_r) = 13.1

Area = $256 \text{ } \mu\text{m}^2$ ($16 \text{ } \mu\text{m} \times 16 \text{ } \mu\text{m}$)

Minority carrier diffusion coefficient, D_p , in the p side of $5 \text{ cm}^2/\text{Sec}$

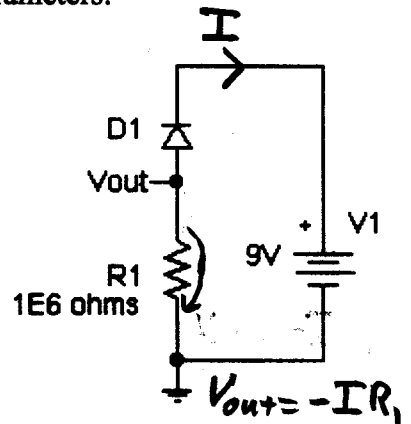
Minority carrier diffusion length, L_p , in the p-side of $0.1 \text{ } \mu\text{m}$

p-type doping of $1 \times 10^{19} \text{ cm}^{-3}$

Minority carrier diffusion coefficient, D_n , in the n side of $10 \text{ cm}^2/\text{Sec}$

Minority carrier diffusion length, L_n , in the n-side of $0.5 \text{ } \mu\text{m}$

n-type doping of $1 \times 10^{15} \text{ cm}^{-3}$.



The diode is to be used as a photodetector biased with the circuit shown. Find the value of the output voltage, V_{out} , for (a. 10-points) dark conditions where there is no light and (b. 10-points) for lighted conditions when a generation rate of 1×10^{19} electron-hole pairs/ $\text{cm}^3 \cdot \text{Second}$ illuminates the diode.

a.) Dark: $I = I_0 (e^{V/0.0259} - 1)$

But clearly, D1 can only be reverse biased so, $I \approx -I_0$

$$I_0 = qA \left(\frac{D_n}{L_n} \frac{n_i^2}{N_A} + \frac{D_p}{L_p} \frac{n_i^2}{N_D} \right)$$

$$= 1.6 \times 10^{-19} (0.0016 \text{ cm} \times 0.0016 \text{ cm}) \left(\frac{10 \text{ cm}^2/\text{s}}{5 \times 10^{-5} \text{ cm}} \frac{(2 \times 10^6)^2 \text{ cm}^{-6}}{1 \times 10^{19} \text{ cm}^{-3}} + \frac{5 \text{ cm}^2/\text{s}}{1 \times 10^{-5} \text{ cm}} \frac{(2 \times 10^6)^2 \text{ cm}^{-6}}{1 \times 10^{15}} \right)$$

$$= 8.2 \times 10^{-22} \text{ A}$$

$$V_{out} = -I R_1 = +I_0 R_1$$

$$V_{out} = 8.2 \times 10^{-16} \text{ volts}$$

Extra work can be done here, but clearly indicate with problem you are solving.

$$\begin{aligned} \text{b.) Light: } I &= I_{\text{dark}} + I_{\text{Light}} \\ &= -I_0 - qA (L_n + W + L_p) G_L \end{aligned}$$

we need w ,

$$W = \sqrt{\frac{2 k_B \epsilon_0}{q} \left(\frac{N_A + N_D}{N_A N_D} \right) (V_{bi} - V_A)}$$

$$V_{bi} = \frac{k_B T}{q} \ln \left(\frac{N_A N_D}{n_i^2} \right)$$

$$V_{bi} = 1.28 \text{ volts}$$

$$\Rightarrow W = \sqrt{\frac{2(1.31)(8.854 \times 10^{-14} \text{ F/cm})}{(1.6 \times 10^{-19})} \left(\frac{1 \times 10^{19} + 1 \times 10^{15}}{(1 \times 10^{19})(1 \times 10^{15})} \right) (1.28 + 0)}$$

$$W = 0.000386 \text{ cm } (3.86 \mu\text{m})$$

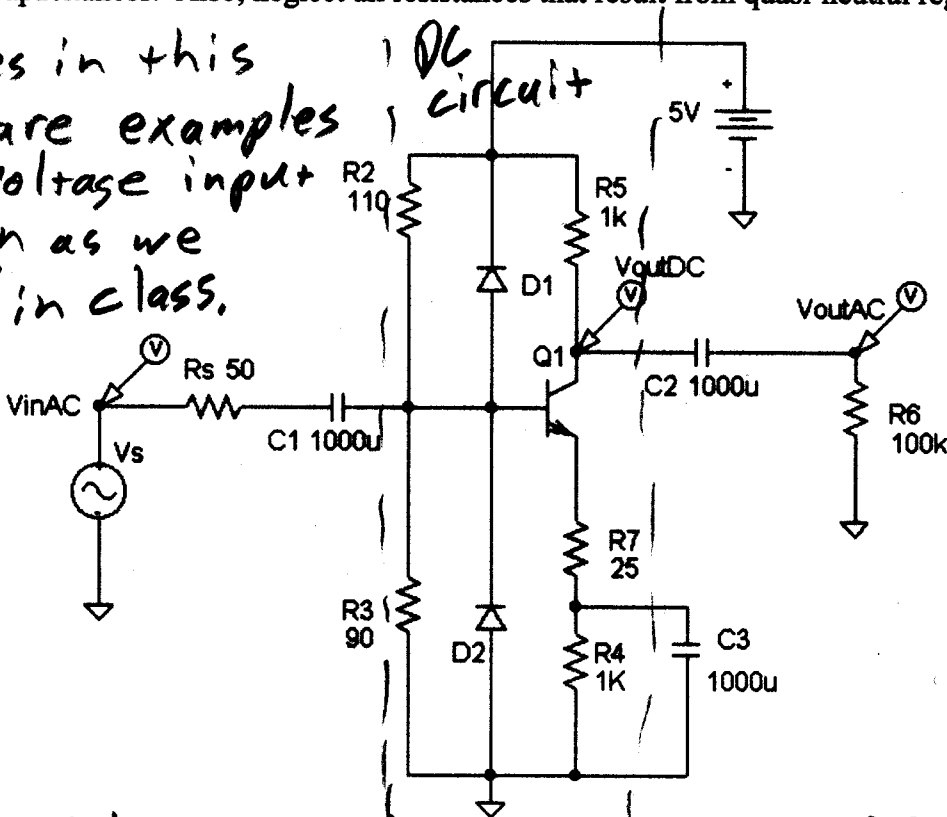
$$\begin{aligned} \text{so } I &= -I_0 - 1.6 \times 10^{-19} (.0016)^2 (1 \times 10^{-5} \text{ cm} + 3.86 \times 10^{-4} \text{ cm} \\ &\quad + 5 \times 10^{-5} \text{ cm}) 1 \times 10^{19} \text{ cm}^{-3} / \text{s} \\ &= -1.83 \times 10^{-9} \end{aligned}$$

$$V_{\text{out}} = -I R_i$$

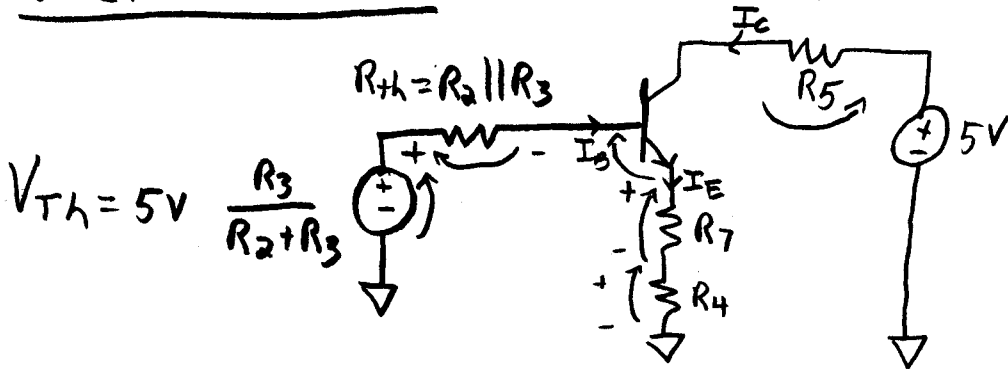
$$V_{\text{out}} = 1.83 \text{ mV}$$

8.) (40-points) Given the following "video amplifier circuit" and BJT Parameters, what is the AC voltage gain, V_{outAC}/V_{inAC} ? Assume: $\beta_{DC}=100$, Early voltage is infinite, turn on voltages for all forward biased junctions are 0.6 V. You may assume all capacitors are very large values and are thus, AC shorts. Additionally consider the circuit to be operated at low frequencies where you can neglect all small signal capacitances. Also, neglect all resistances that result from quasi-neutral regions.

The diodes in this circuit are examples of over-voltage input protection as we discussed in class.



D.C. Solution: Assume $D1 + D2$ are off



$$0 = V_{th} - I_B R_{th} - V_{BE} - I_E R_7 - I_E R_4$$

$$5 \left(\frac{90}{90+110} \right) = I_B (49.5) + 0.6 - (100+1) I_B (25+1000)$$

$$I_B = \frac{1.65V}{49.5 + 101(1025)} = 15.9 \mu A$$

$$I_C = 1.59 mA$$

$$I_E = \left(\frac{100+1}{100} \right) I_C = 1.61 mA$$

Extra work can be done here, but clearly indicate with problem you are solving.

$$V_c = 5 - I_c R_5$$
$$= 5 - (1.59e-3)(1e3)$$

$$V_c = 3.41 \text{ V}$$

$$V_B = V_{th} - I_B R_{th}$$
$$= 5 \left(\frac{90}{90+110} \right) - (15.9e-6) 49.5$$

$$V_B = 2.25 \text{ V}$$

$$V_E = I_E (R_4 + R_7)$$
$$= (1.61e-3) (1025)$$
$$= 1.65 \text{ V}$$

Forward Active is correct assumption.

D_1 is off since $V_B < 5 \text{ V}$

D_2 is off since $V_B > 0 \text{ V}$

Small Signal Parameters:

$$g_m = \frac{I_c}{V_T} = \frac{1.59e-3}{0.0259} = 0.0614 \text{ S} \quad (0)$$

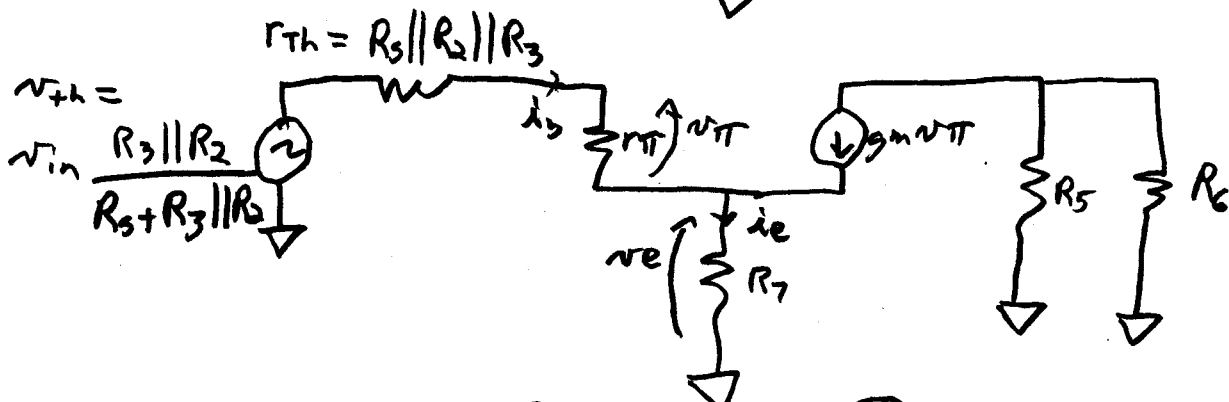
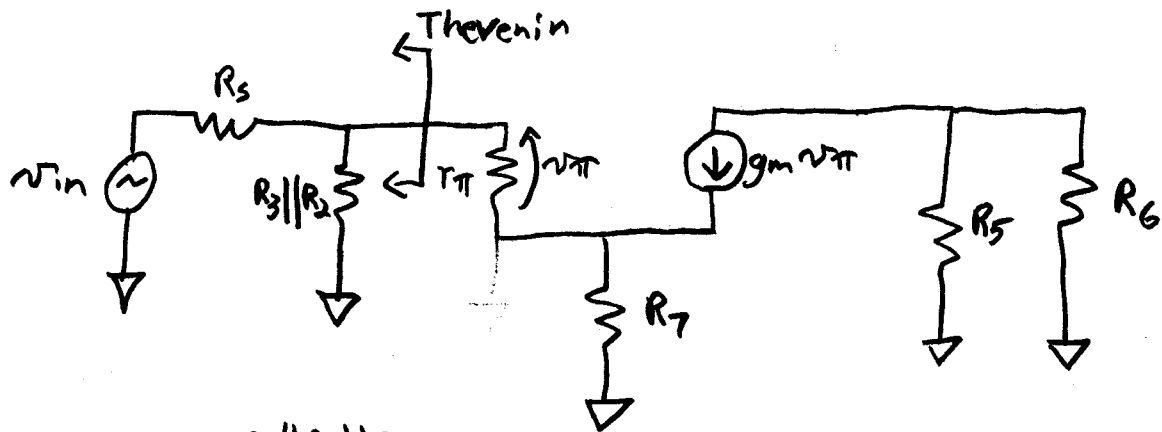
$$r_{\pi} = \frac{\beta}{g_m} = \frac{100}{0.0614} = 1.629 \text{ k}\Omega \quad (1)$$

$$r_o = \frac{V_A + V_{CE}}{I_c} = \frac{\infty}{I_c} = \infty$$

Diode: $g_d = \frac{I_D + I_S}{V_T} = \frac{-I_S + I_S}{V_T} = 0$

$$r_d = \frac{1}{g_d} = \infty$$

A.C. Solution:



$$A_v = \overset{(1)}{\left(\frac{v_{out}}{v_{\pi}}\right)} \overset{(2)}{\left(\frac{v_{\pi}}{v_{th}}\right)} \overset{(3)}{\left(\frac{v_{th}}{v_{in}}\right)}$$

Term 1.) $v_{out} = -g_m v_{\pi} (R_5 || R_6)$

$$\frac{v_{out}}{v_{\pi}} = -g_m (R_5 || R_6) \quad \text{check: unitless} \checkmark$$

Term 3.) $v_{th} = v_{in} \frac{R_3 || R_2}{R_3 || R_2 + R_s}$

$$\frac{v_{th}}{v_{in}} = \frac{R_3 || R_2}{R_3 || R_2 + R_s} \quad \text{check: unitless} \checkmark$$

$$= 0.497 \text{ v/v}$$

(6)

Extra work can be done here, but clearly indicate with problem you are solving.

Term 2.) $v_{zh} = i_b (R_5 \parallel R_2 \parallel R_3) + v_{\pi} + v_e$

$v_{zh} = \frac{v_{\pi}}{r_{\pi}} (R_5 \parallel R_2 \parallel R_3) + v_{\pi} + \left(\frac{v_{\pi}}{r_{\pi}} + g_m v_{\pi} \right) R_7$

$$\frac{v_{\pi}}{v_{zh}} = \frac{1}{\frac{R_5 \parallel R_2 \parallel R_3}{r_{\pi}} + 1 + R_7 \left(\frac{1}{r_{\pi}} + g_m \right)}$$

$$= 0.3898 \text{ v/v} \quad (1)$$

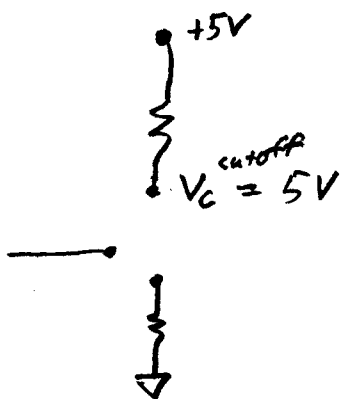
$$A_v = (-60.8)(0.3898)(0.497)$$

$$A_v = -11.8 \text{ v/v}$$

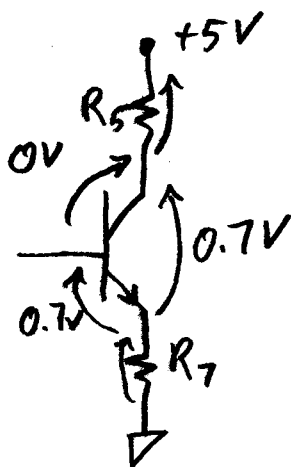
Bonus of 15 points total:

In the last problem, what is the minimum and maximum "Large signal" output swing possible before distortion begins? Note: I am asking for the "actual" voltage swing, not the simpler "worst case" voltage swing.

1st extreme: Onset of cutoff:



2nd extreme: Onset of saturation:



$$5V = I_E R_7 + 0.7 + I_C R_5$$

$$4.3V = \left(\frac{100+1}{100} R_7 + R_5 \right) I_C$$

$$I_C = 4.19 \text{ mA}$$

$$V_C = 5V - I_C R_5$$

$$V_C = 0.806 \text{ V}$$

